

Wave Information Sensitivity for Upper Ocean Structure under Typhoon Condition

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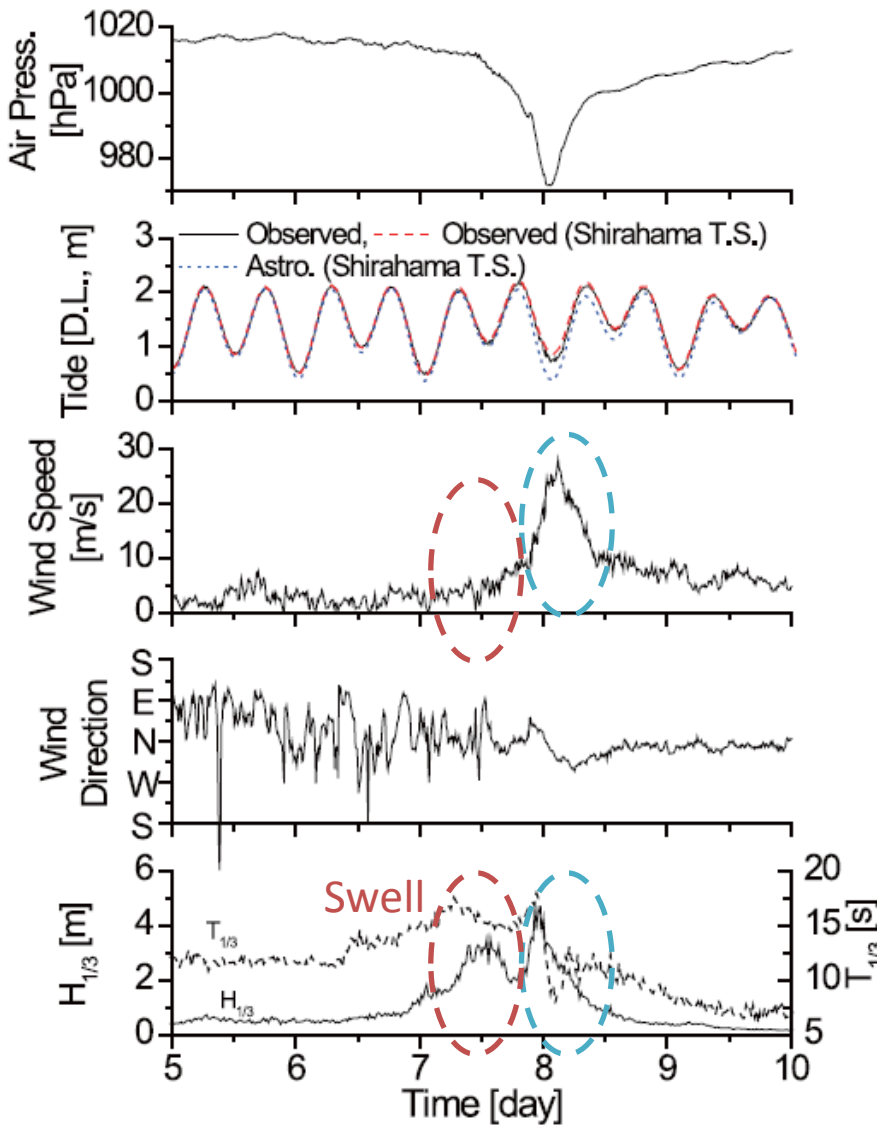
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Hajime Mase

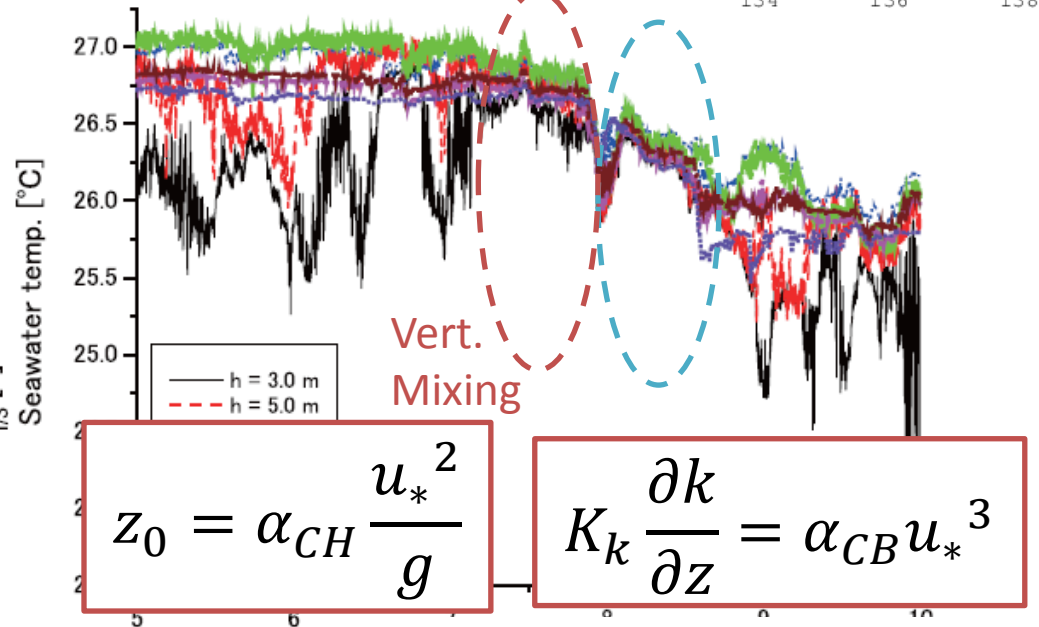
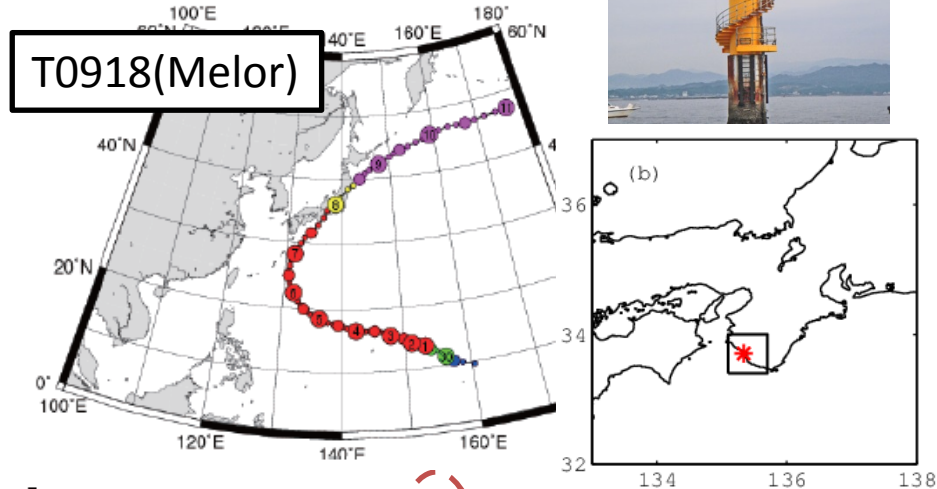
USGS

J.C. Warner

Motivation



T0918(Melor)



$$z_0 = \alpha_{CH} \frac{u_*^2}{g}$$

$$K_k \frac{\partial k}{\partial z} = \alpha_{CB} u_*^3$$

-> Wave information?

Methodology

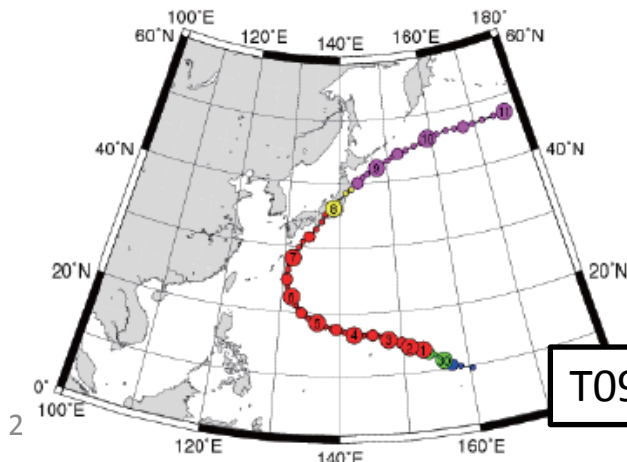
- Momentum bulk formulas

$$z_0 = \max\left(\frac{\alpha_{CH}}{g}(u_*)^2, z_{0min}\right)$$

$$\frac{z_0}{H_s} = A \left(\frac{H_s}{L_p}\right)^B$$

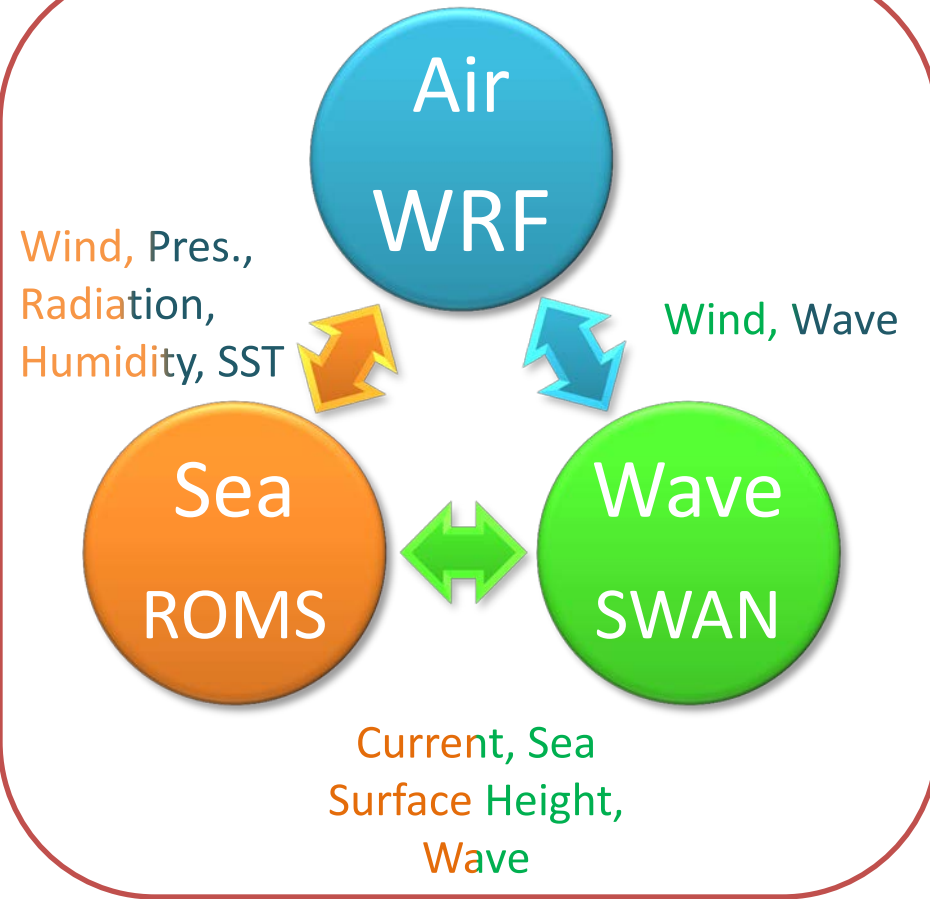
$$\frac{z_0}{L_p} = \frac{C}{\pi}(u_*/C_p)^D$$

$$\frac{z_0}{H_s} = E(u_*/C_p)^F$$



T0918(Melor)

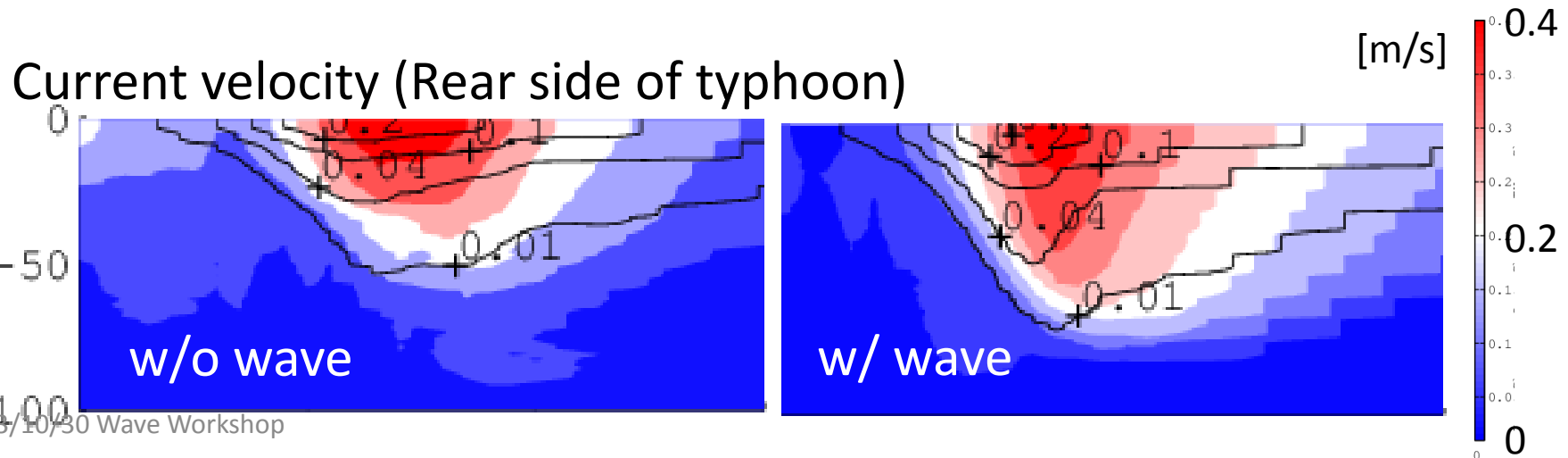
Coupling Model



+ Air side roughness + Sea side roughness
+ TKE flux

Conclusions

- Numerical experiments for typhoon using four bulk formulas were carried out.
- Sensitivity of bulk formulas were found
 - Distribution according to direction from typhoon center
 - Large influence of wave information on current velocity, sensible and latent heat, and vertical wind profile



Typical Proposed Bulk Formulas at Sea Surface

1. Charnock (1955): Friction Velocity

$$z_0 = \max\left(\frac{\alpha_{CH}}{g}(u_*)^2, z_{0min}\right)$$

$$\alpha_{CH} = 0.018$$

$$\alpha_{CH} = 0.011 + 0.125(0.018 - 0.011)(u - 10.0)$$

$$\alpha_{CH} = 0.011$$

Air side Roughness

$$\text{for } 18.0 < u$$

$$\text{for } 10.0 < u < 18.0$$

$$\text{for } u < 10.0$$

2. Taylor and Yelland (2001): Wave Slope

$$\frac{z_0}{H_s} = A \left(\frac{H_s}{L_p} \right)^B$$

$$A = 1200, B = 4.5$$

H_s : Wave height, L_p : Wave length

WRF default setting:
 $z_0 = \max(z_{0CH}, 1.59 \times 10^{-5})$
 $\alpha_{CH} = 0.018$

3. Oost (2002): Wave age, Wave length

$$\frac{z_0}{L_p} = \frac{C}{\pi} (u_*/C_p)^D$$

$$C = 25.0, D = 4.5$$

C_p : Wave velocity

4. Drennan (2003): Wave age, Wave height

$$\frac{z_0}{H_s} = E (u_*/C_p)^F$$

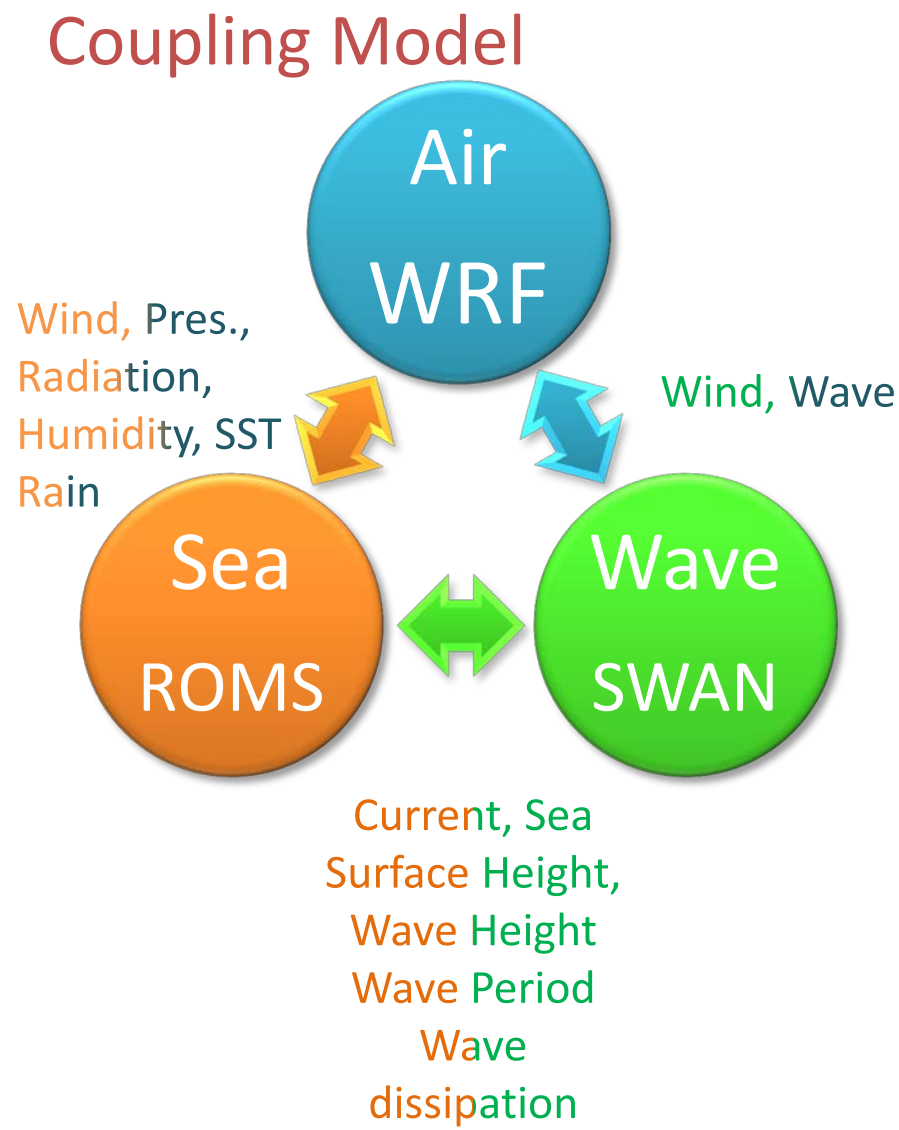
$$E = 3.35, F = 3.4$$

$$u_* = \frac{K u_{ref}}{\log(z_{ref}/z_0)}$$

$$\tau = \rho_a u_*^2$$

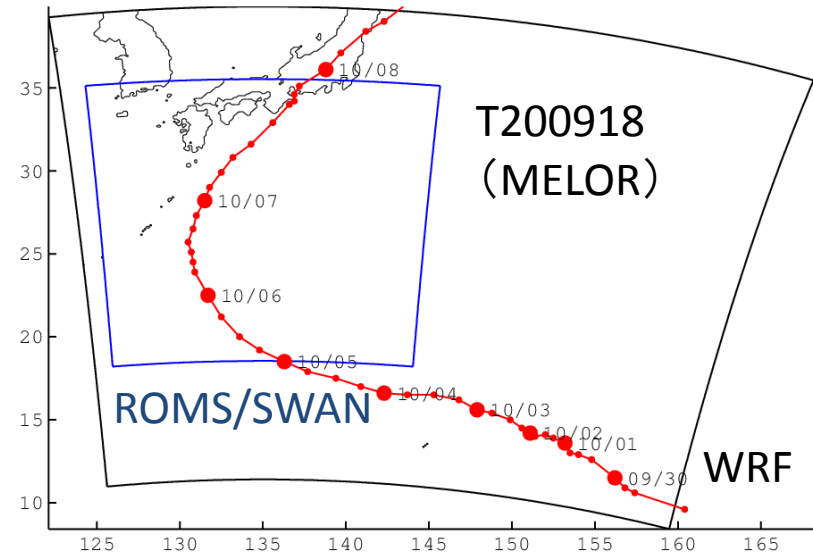
Model Setup

- Initial, Boundary Condition
 - WRF
 - NCEP FNL (Final) Operational Global Analysis data
 - Resolution: 1 degree, 6 hour
 - ROMS
 - JCOPE2 (JAMSTEC)
 - Resolution: 1/12 degree, 1 day
 - SWAN
 - WW3 (NOAA Reanalysis)
 - Resolution: 1/2 degree, 3 hour
- Bulk formula at the surface
 - Air side roughness
 - Ocean side roughness
 - TKE flux



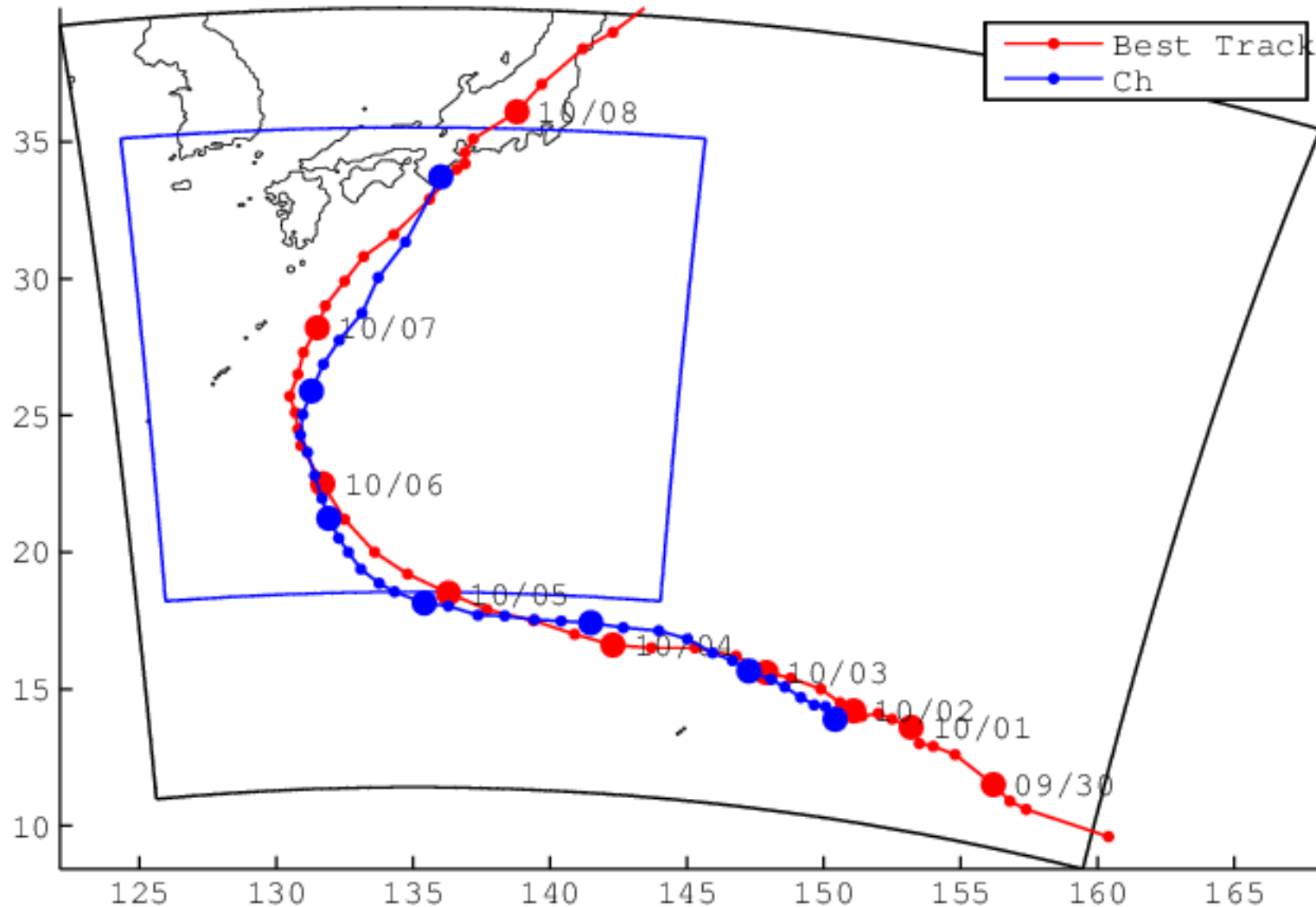
Model Setup for TC Melor (2009)

- Period
 - 2009/9/30 – 10/8
 - Coupling Interval: 600s
- Domain

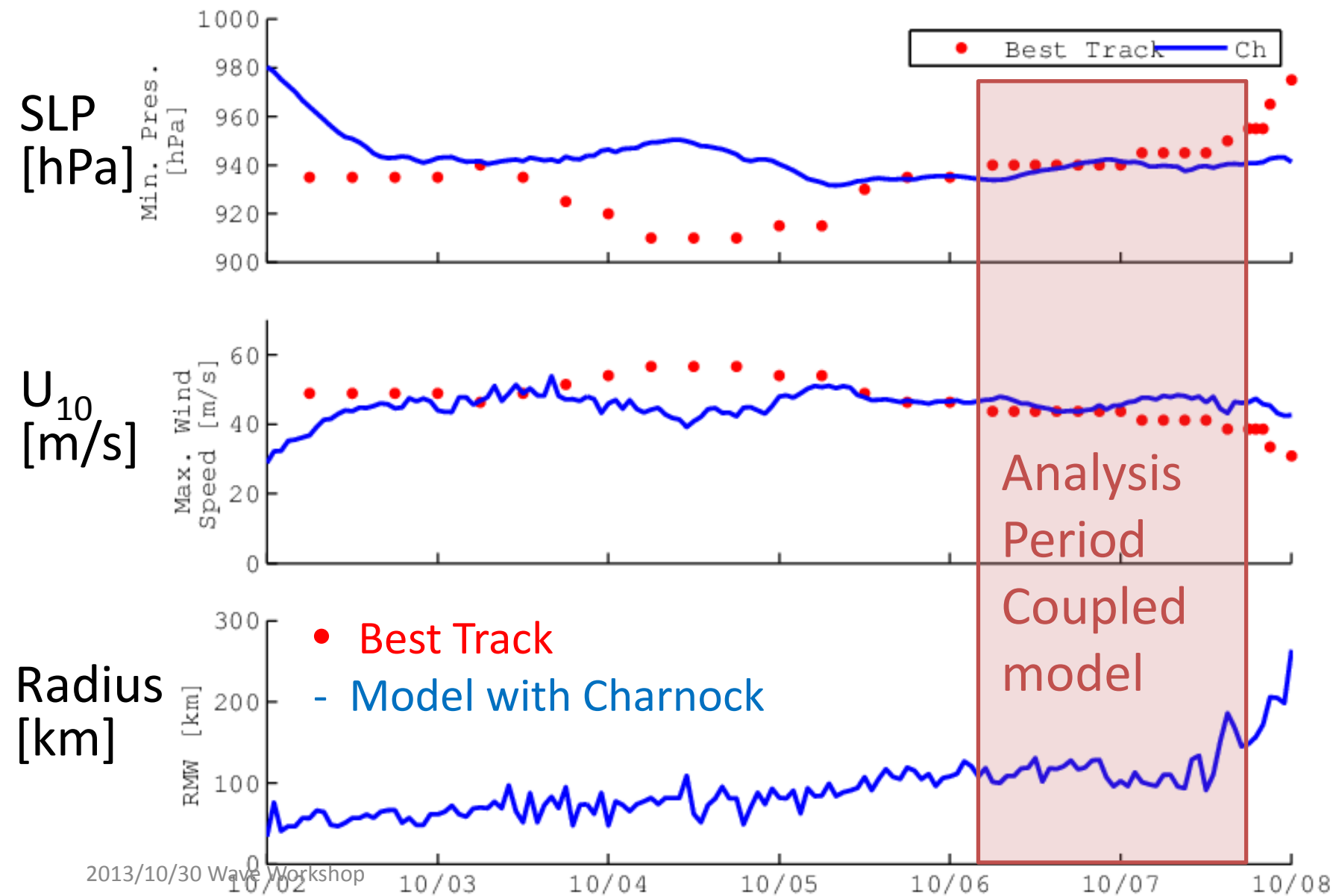


	Resolution	Horizontal grids	Vertical grids Directions etc.	Dt [s]
WRF	12km	338x270	40	50
ROMS		195x190	40	40
SWAN			Dir.: 24 Freq.: 24 (0.05-0.5Hz)	75

Comparison between Best Track and CT



Comparison between Best Track and CT



Results

Air side roughness

Ch: Charnock (Friction velocity)

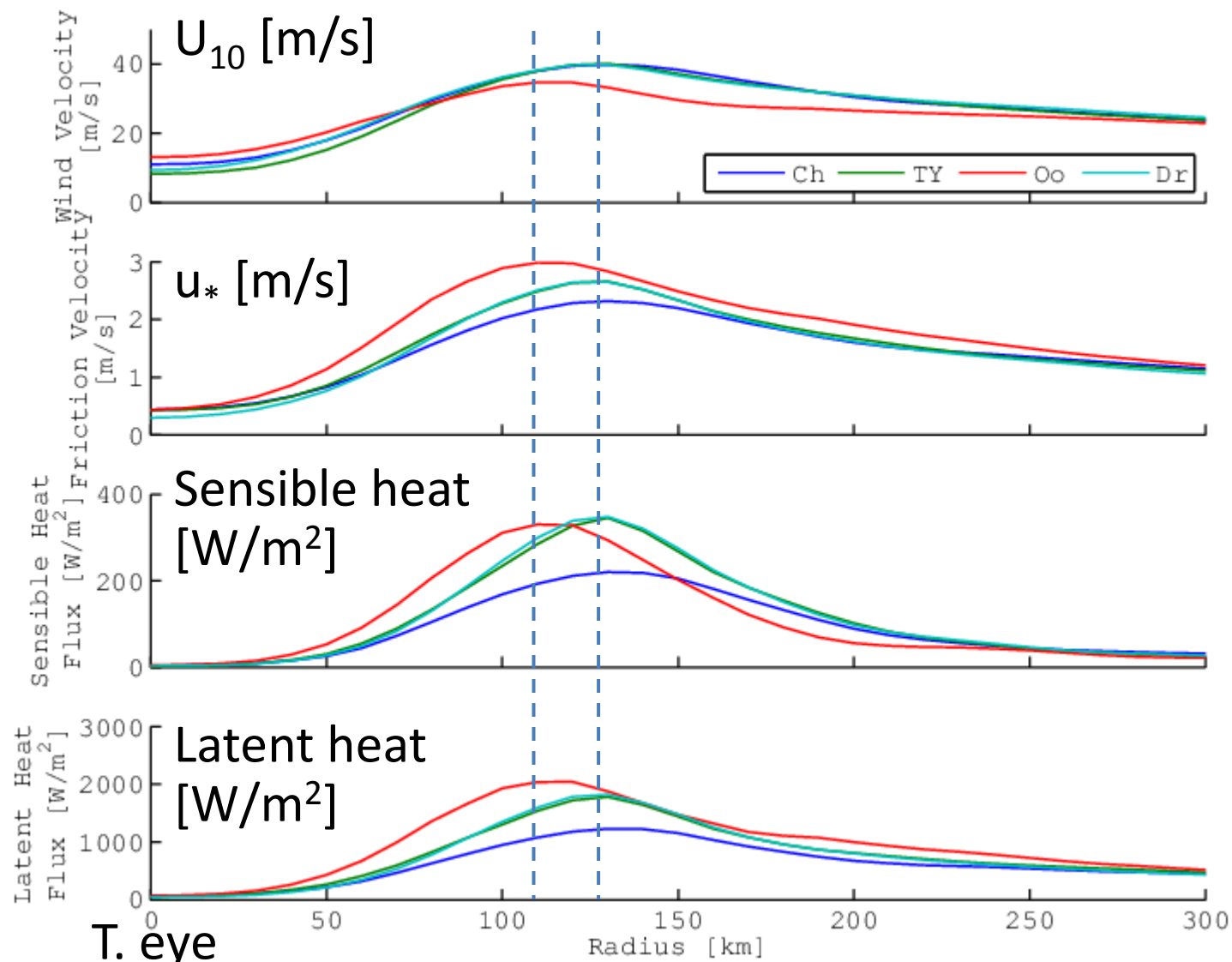
TY: Taylor and Yelland (Wave slope)

Oo: Oost (Wave age – Wave length)

Dr: Drennan (Wave age – Wave height)

Friction Velocity, Sensible/Latent heat flux (time and direction averaged)

2009/10/6 18:00 – 10/7 00:00 UTC



Z0 by

Charnock

Taylor-Yelland

Oost

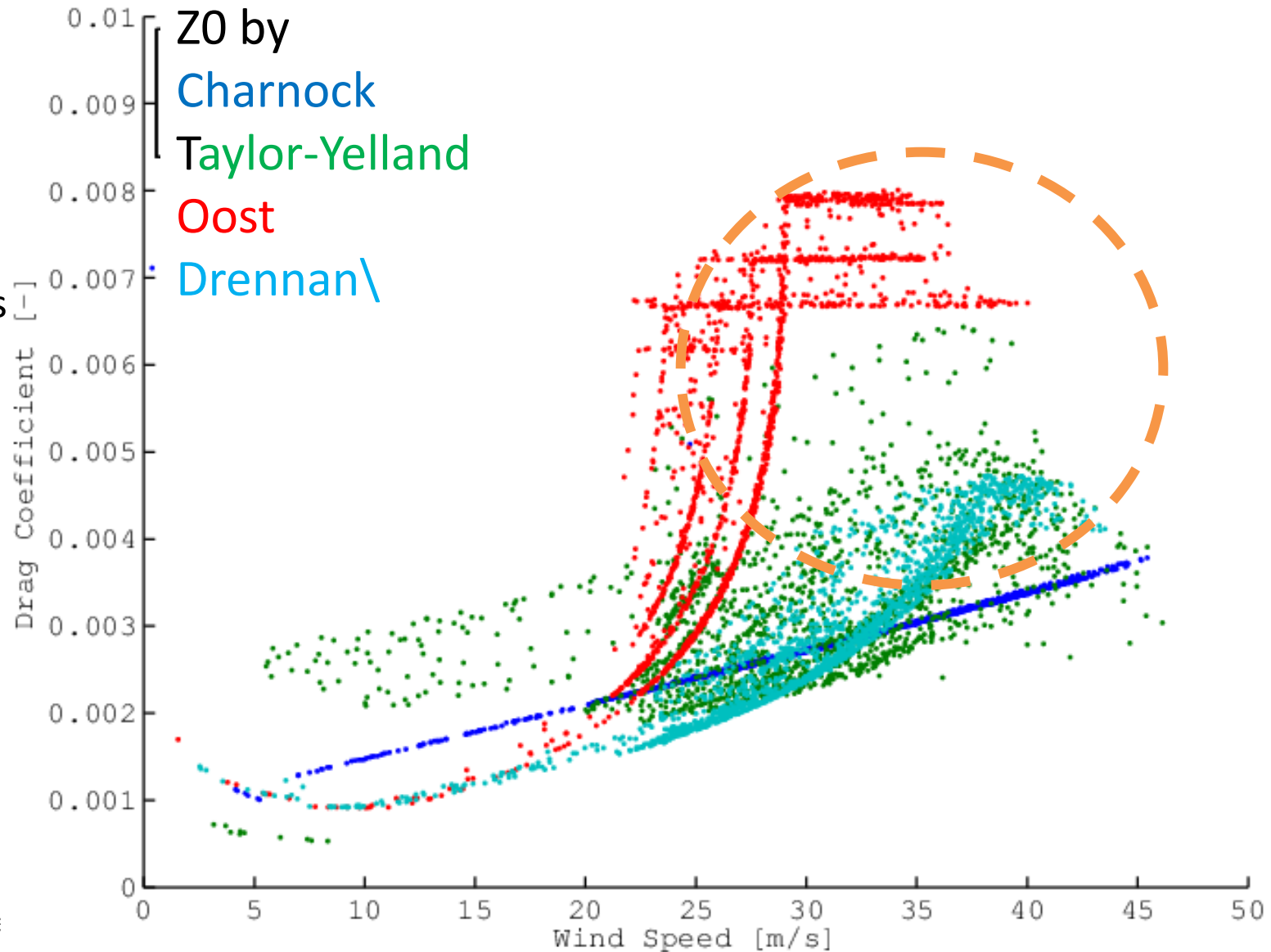
Drennan

Oost formula estimates peak value at closer to center of typhoon.

Wave based formulas estimate large friction velocity and heat flux.

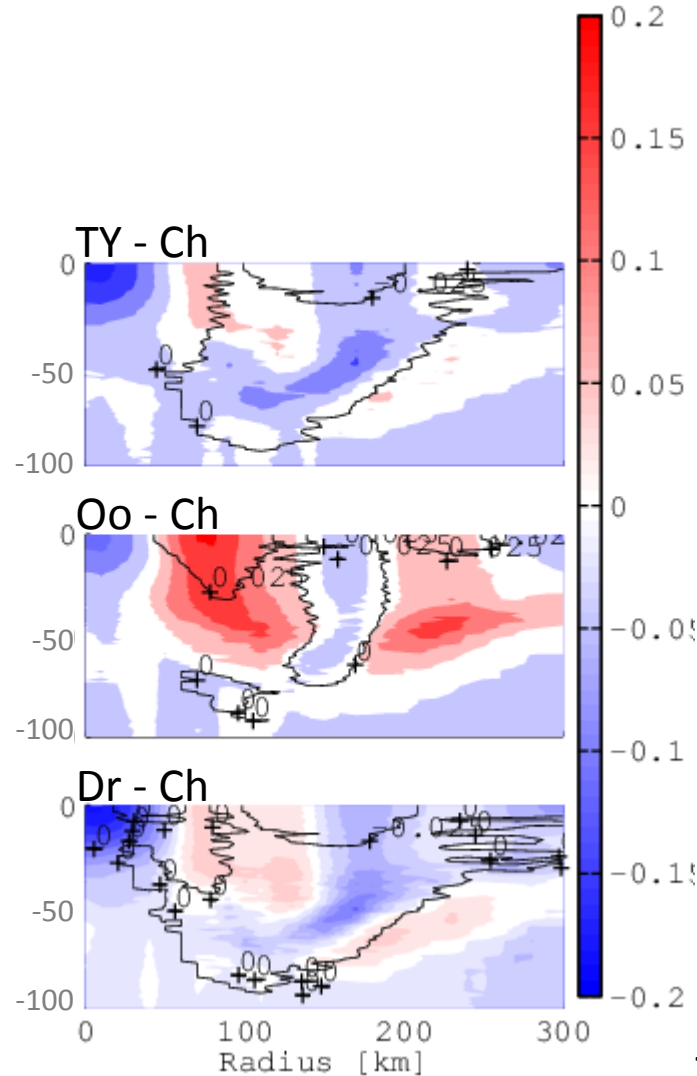
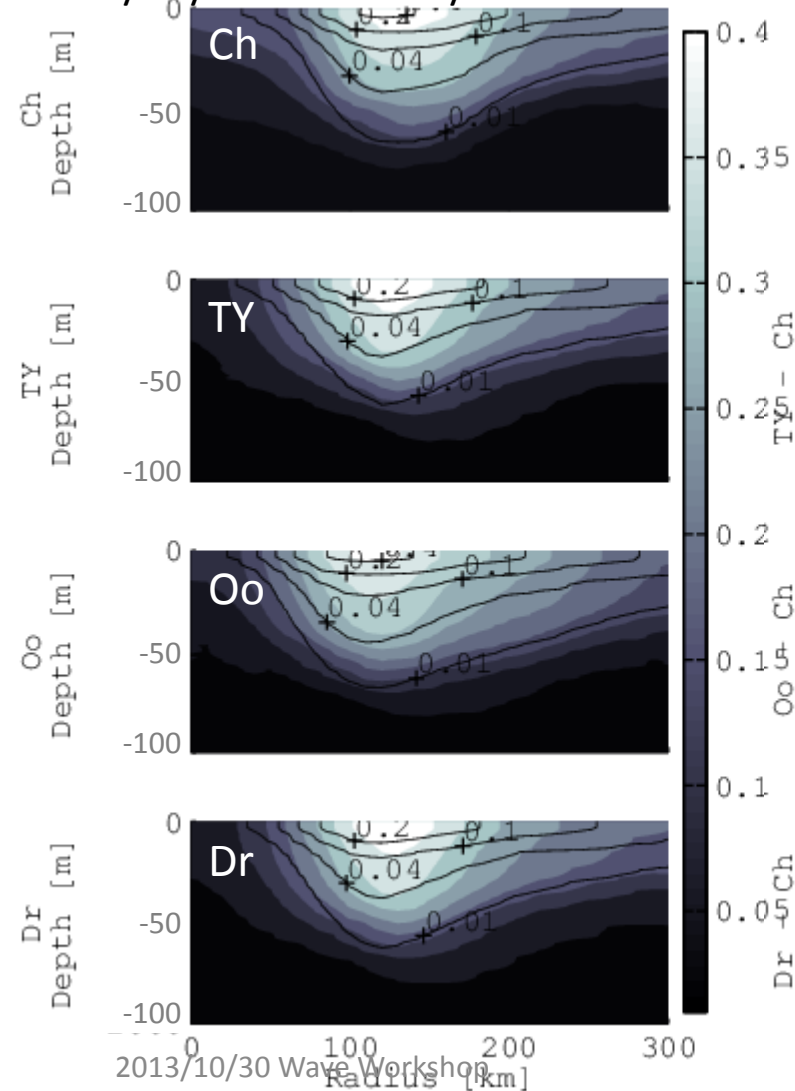
Internally Calculated Drag Coefficient

Drag coefficient is good indicator how roughness influence on the momentum transfer at air-sea interface.



Current Velocity, TKE (time and direction averaged)

2009/10/6 18:00 – 10/7 00:00 UTC

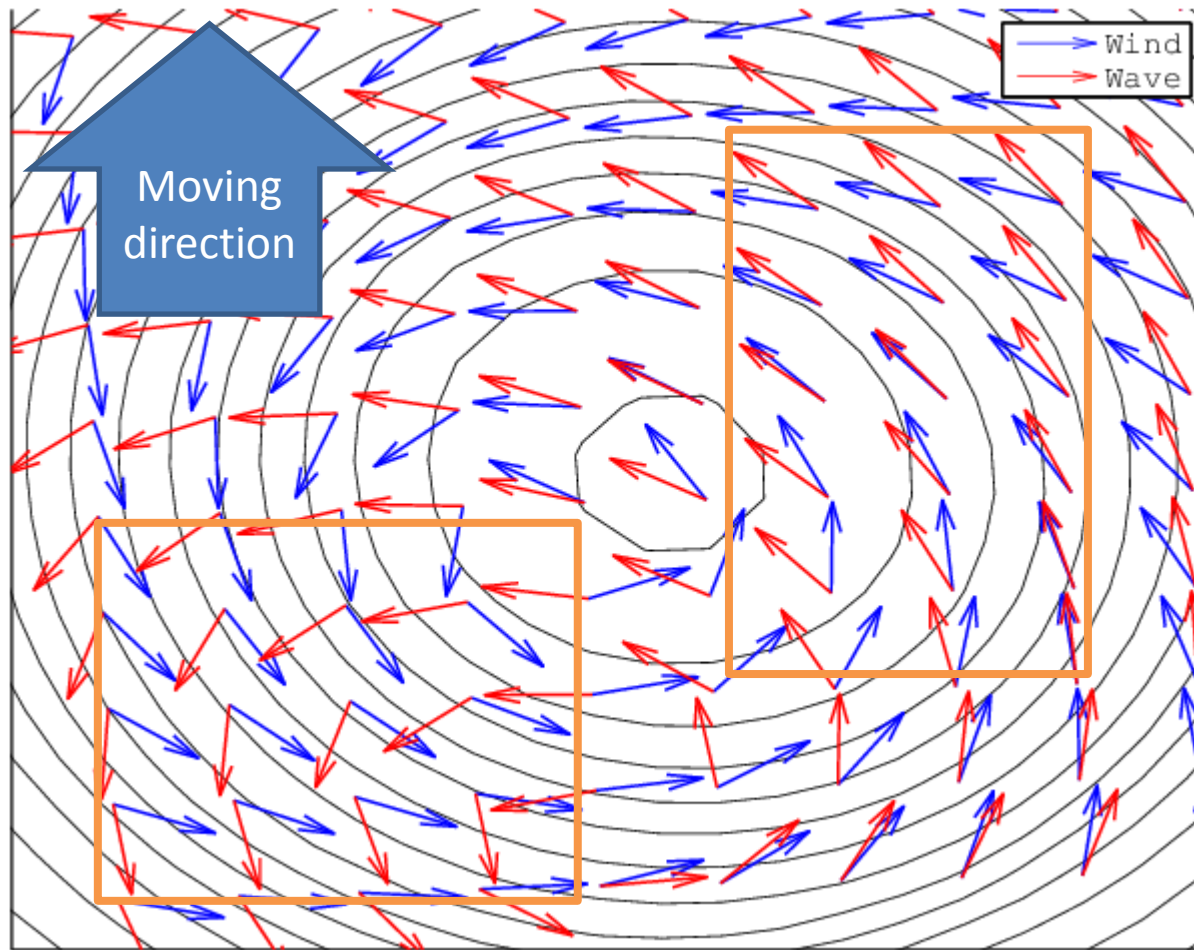


Ch, TY, Dr
estimate similar
distribution.

Oo
large
current
velocity.

H. Vel.: Shade
TKE: Contour

Wind and Wave Direction around Typhoon Eye

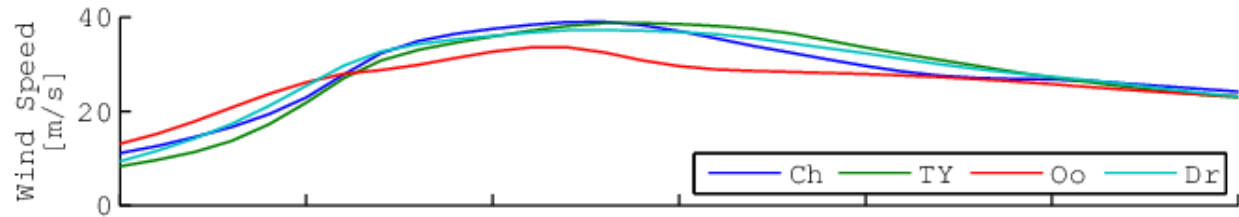


Wave direction agree with wind direction in front side, but disagree in rear side.

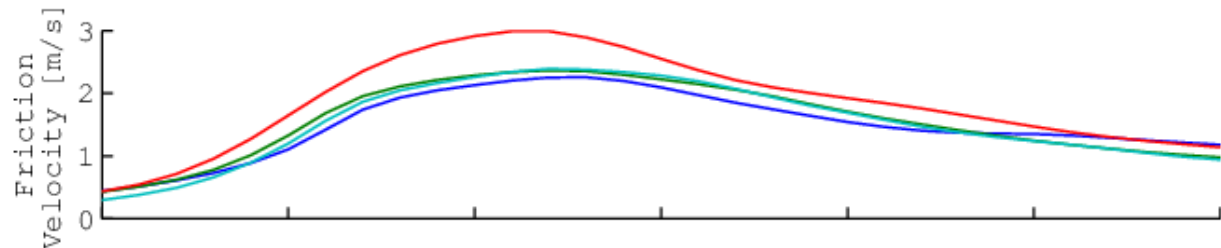
Friction Velocity, Sensible/Latent Heat Flux

2009/10/6 18:00 – 10/7 00:00 UTC (Moving direction : North)

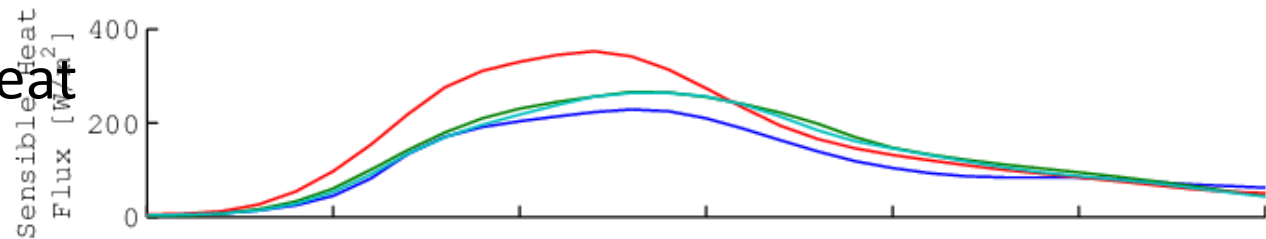
U_{10} [m/s]



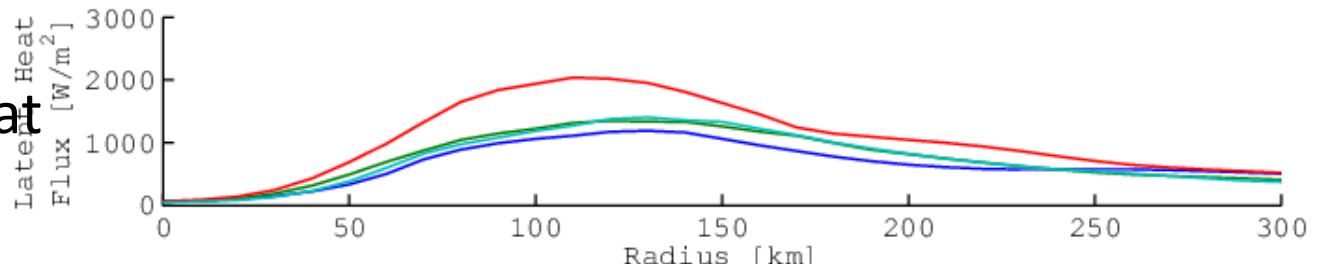
u_* [m/s]



Sensible heat
[W/m²]



Latent heat
[W/m²]

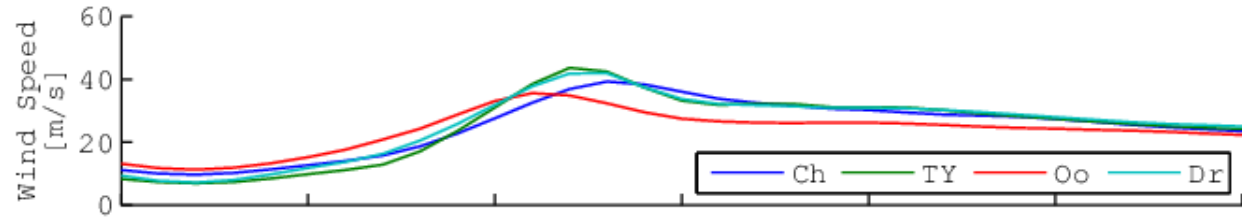


In front side, Ch, TY and Dr estimate similar distribution. In rear side, formulas with wave information estimate large friction velocity and heat flux.

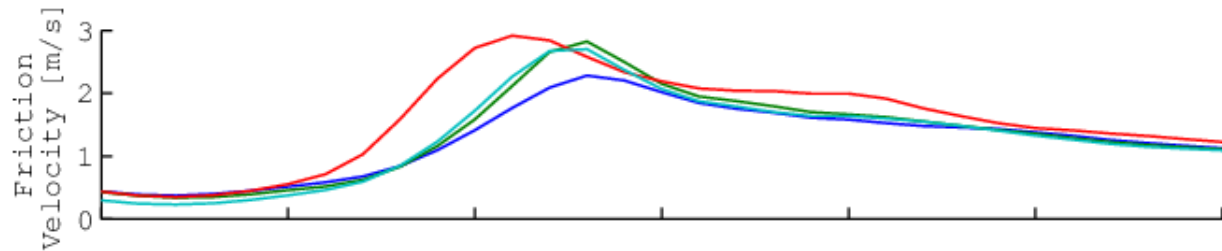
Friction Velocity, Sensible/Latent Heat Flux

2009/10/6 18:00 – 10/7 00:00 UTC (Moving direction : North)

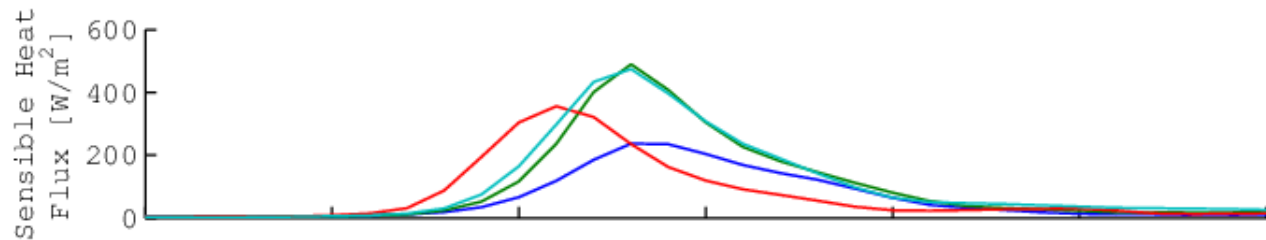
U_{10} [m/s]



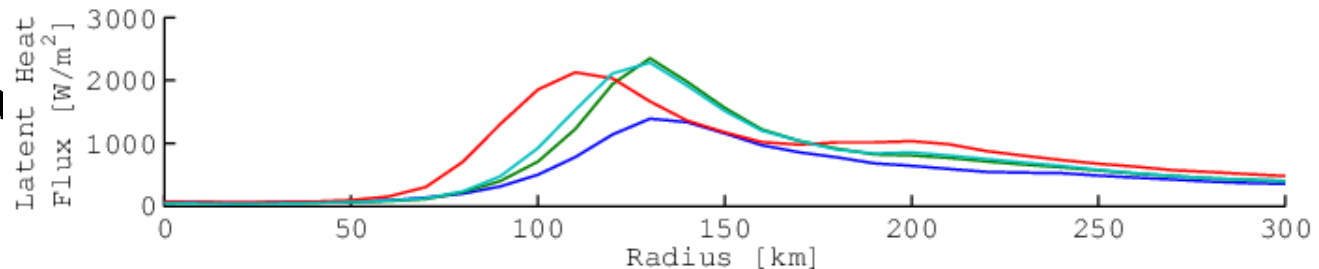
u_* [m/s]



Sensible heat
Flux [W/m²]



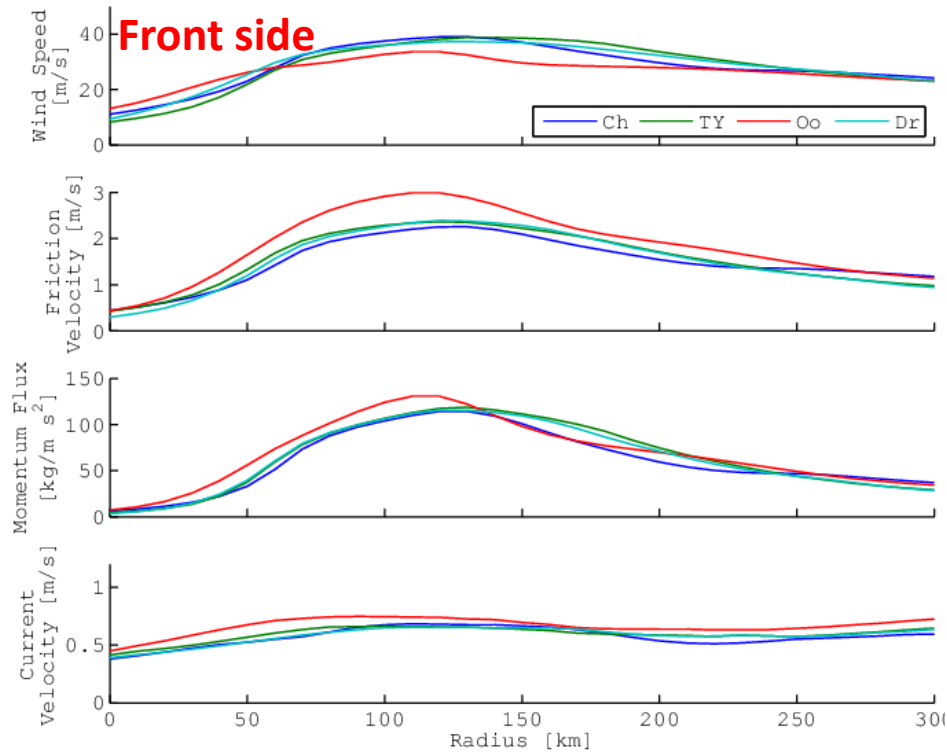
Latent heat
Flux [W/m²]



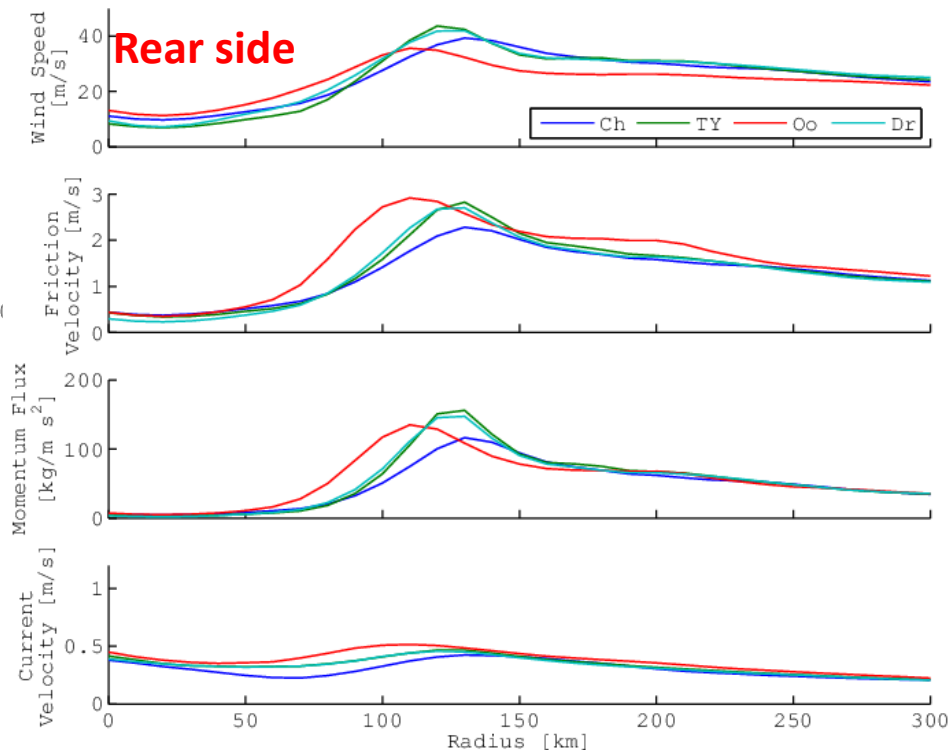
In front side, Ch, TY and Dr estimate similar distribution. In rear side, formulas with wave information estimate large friction velocity and heat flux.

Current Velocity at Sea Surface

2009/10/6 18:00 – 10/7 00:00 UTC



Bulk formulas except Oo estimate **similar distribution in front side**, but wave based formulas estimate 10 – 30 % **larger peak velocity** than wind based formula **in rear side**.

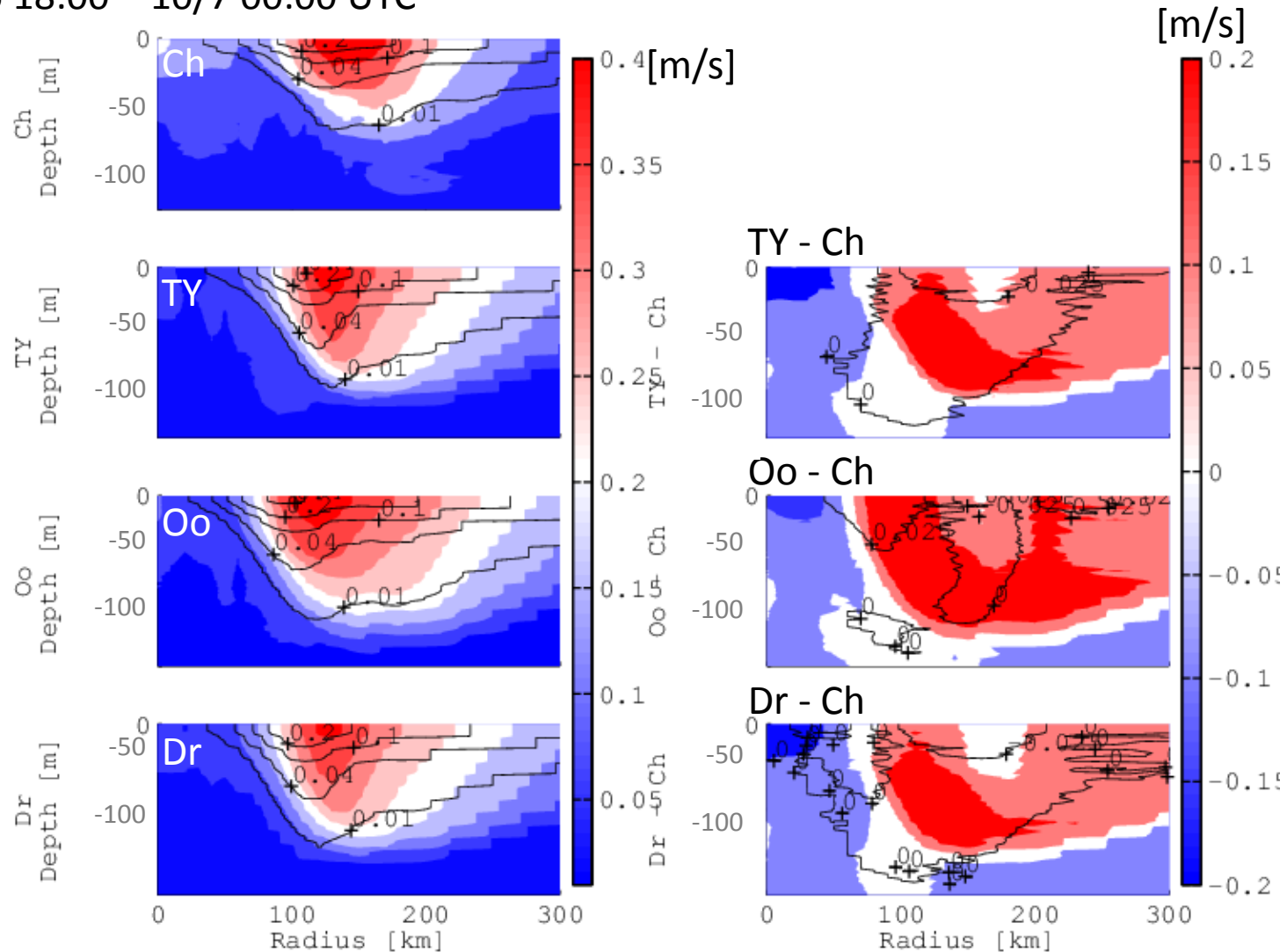


Rear side

Current Velocity, TKE

H. vel.: shaded
TKE: contour

2009/10/6 18:00 – 10/7 00:00 UTC



In rear side, Ch estimates smaller current velocity.

Wave based Formulas estimate wider and deeper current distribution.

Conclusions

- Numerical experiments using four bulk formulas of air side roughness were carried out.
 - Oost formula estimated larger friction velocity than the other formulas.
- Radial direction averaged value from typhoon center
 - Large influence of wave information
 - Friction velocity, sensible and latent heat flux
 - Small influence
 - Typhoon features, wind speed, current velocity, wave
- Distribution according to direction from typhoon center
 - Large influence
 - Front side: Current velocity in the distance from typhoon center
 - Rear side: Friction velocity, heat flux, current velocity
 - Small influence
 - Front side: Almost all parameters
 - Rear side: Wind speed, wave
- Improvement of parameterization gives significant impact on large scale atmosphere and ocean circulation

THE END

Project 2013
Air-sea interaction
measurements for
typhoon

We have accumulated
more than 6 typhoon
data by the tower.
We are going to
compare the model
with observed data.

Ocean observatory Tower
by Kyoto University

2013/10/30 Wave Workshop

